

# Powder diffraction and the Rietveld method

- Principles
- Example

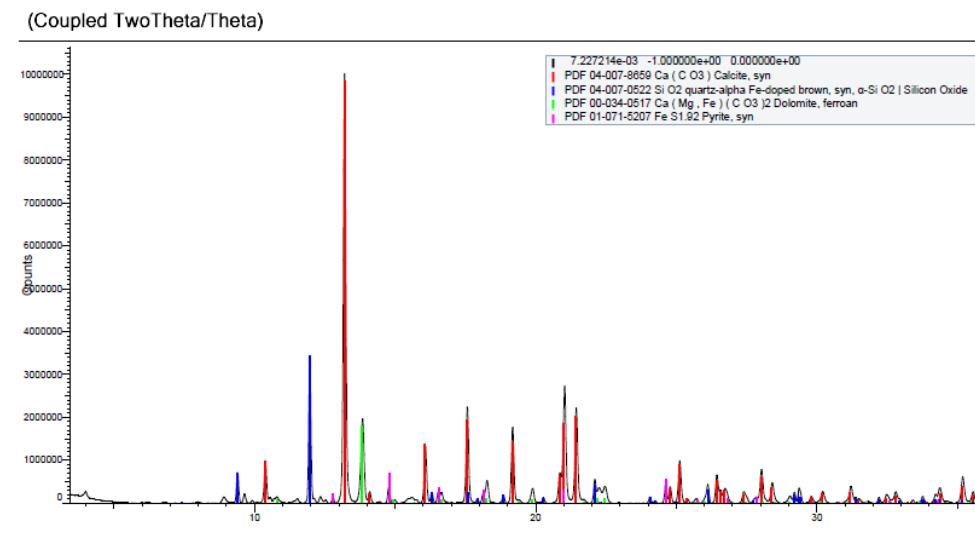
Magnus H. Sørby

*Institute for Energy Technology, Norway*

# Analysis of powder diffraction data

## The fingerprint method

- The position and relative intensities of Bragg peaks are unique for a crystalline phase → a «fingerprint».
- «Automatic» identification of known phases from databases (powder X-ray diffraction!)



# Analysis of powder diffraction data

## Crystal structure determination

Indexing

Find the size and shape of the unit cell



Space group determination

Find the space group or possible space groups

Structure solution

Find the approximate atomic arrangement within the unit cell

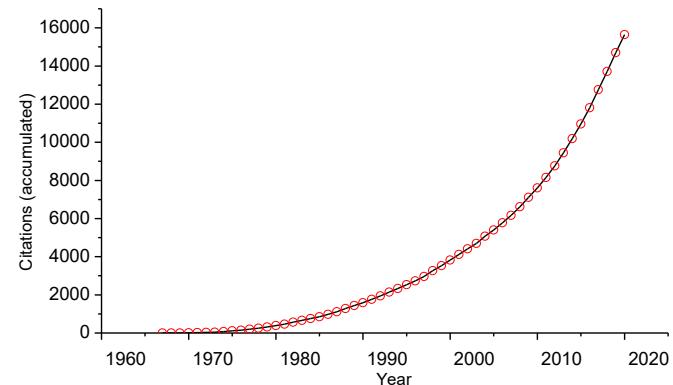
Structure refinement

Make the structure model as accurate as possible

# Analysis of powder diffraction data.

## The Rietveld method

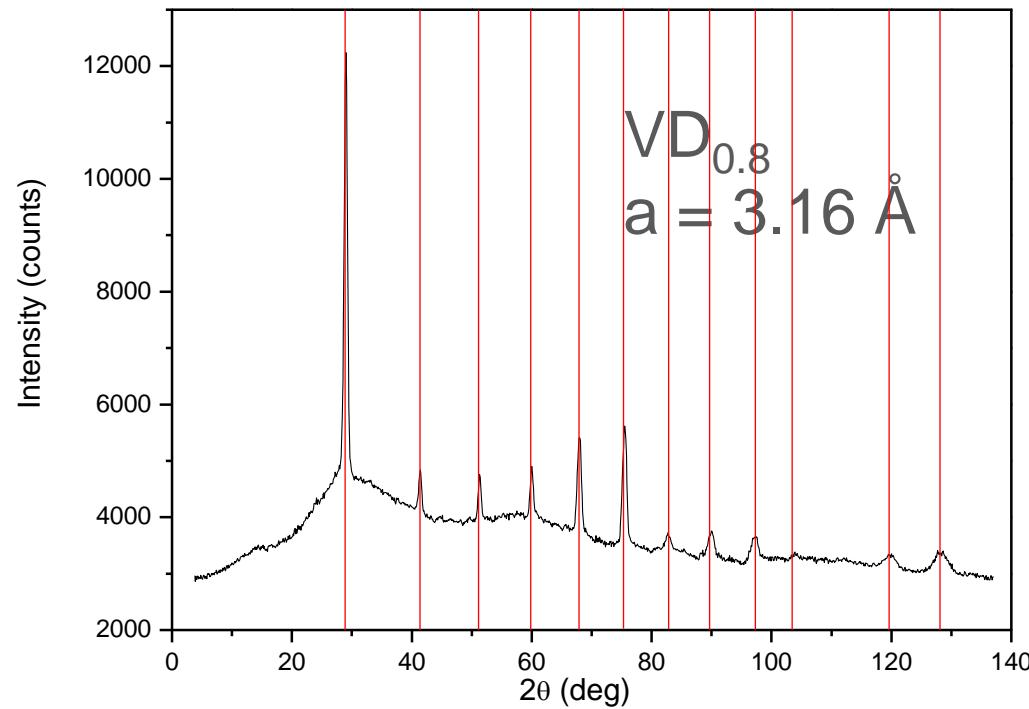
- Introduced by Hugo Rietveld in 1967  
H. M. Rietveld, Acta Cryst. 22 (1967) 151  
H. M. Rietveld, J. App. Cryst. 2 (1969) 65
- Revolutionized analysis of powder diffraction data. Cited 16431 times.



- Developed as a technique for *structure refinement*.

# The Rietveld method

- Developed as a technique for *structure refinement*.

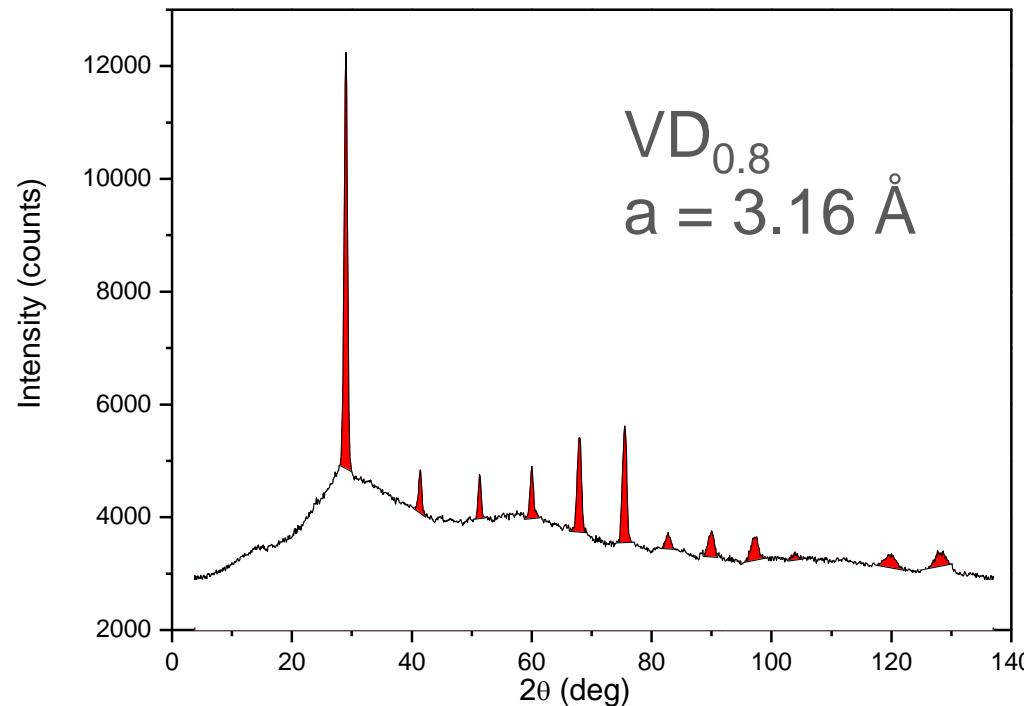


The pre-Rietveld way

hkl	Intensity
110	
200	
211	
220	
310	
....	

# The Rietveld method

- Developed as a technique for *structure refinement*.



The pre-Rietveld way

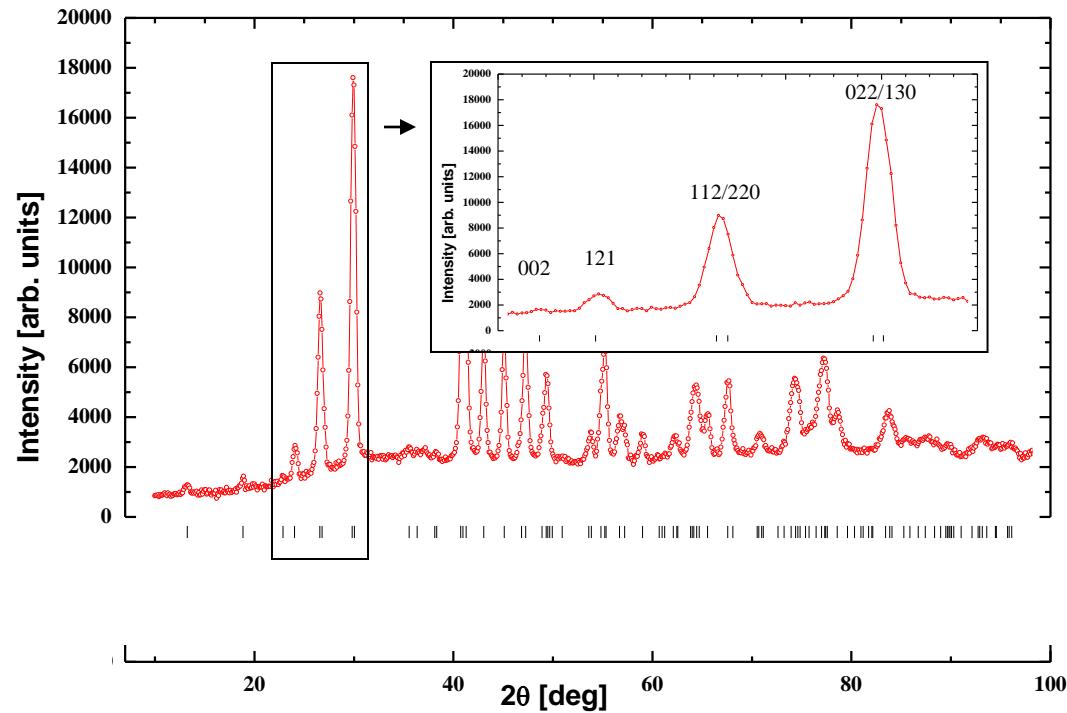
hkl	Intensity
110	1000

$$I_{hkl} \propto \left| \sum_j b_j \cdot e^{2\pi i(hx_j + ky_j + lz_j)} \right|^2$$

310	285
.....	.....

# The Rietveld method

- Developed as a technique for *structure refinement*.



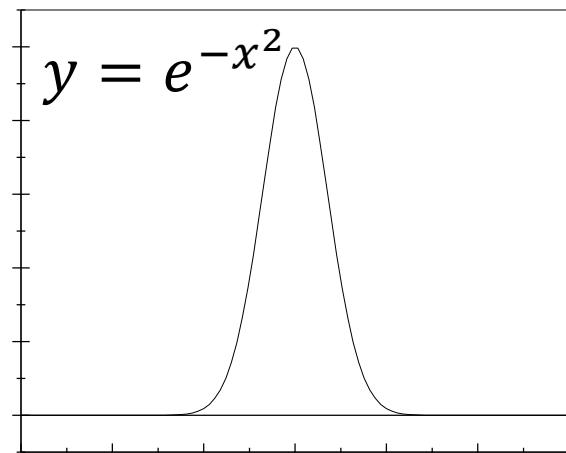
The pre-Rietveld way

hkl	Intensity
101	23
110	34
002	10
121	120
112+220	450
022+130	1000

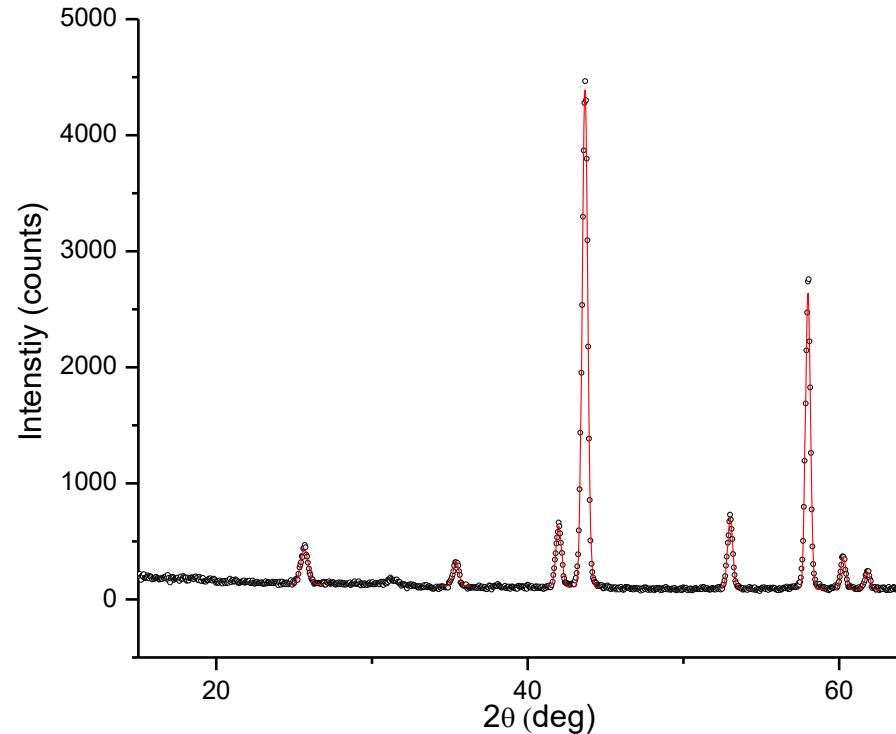
# The Rietveld method

Rietveld's observations:

Well-resolved Bragg- peaks in his PND data had the shape of Gaussian curves.



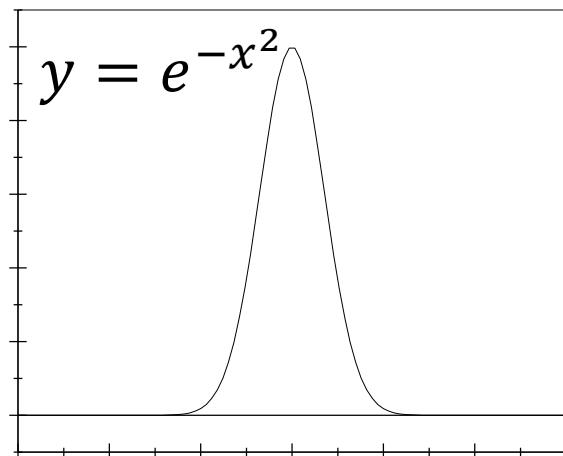
The Gaussian curve



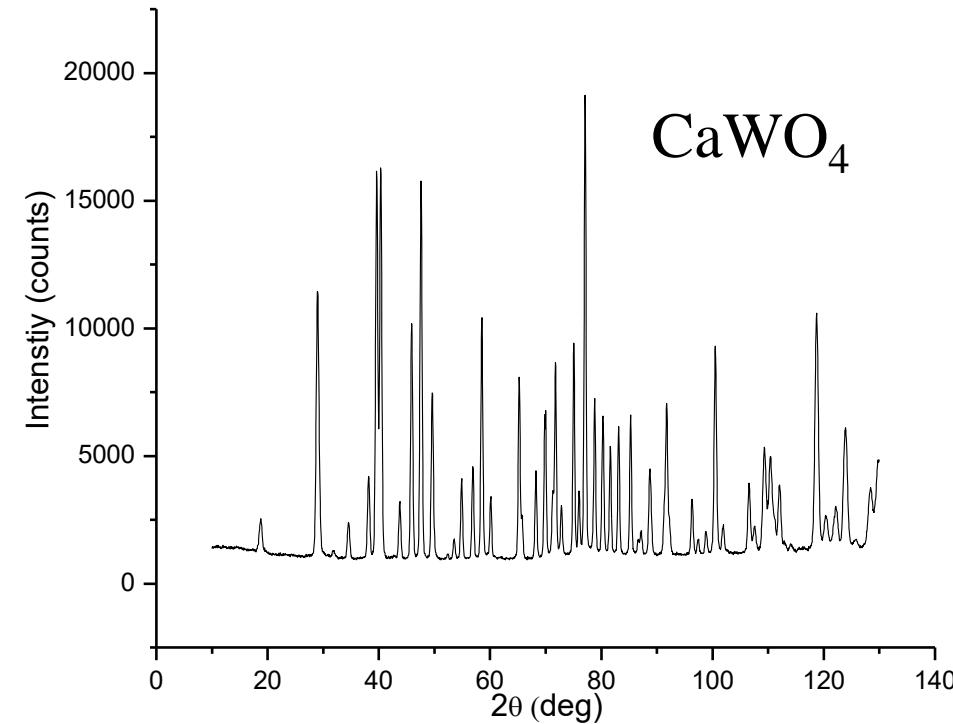
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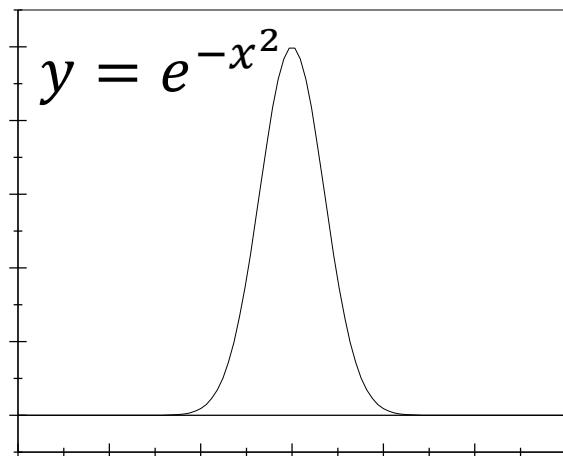
The Gaussian curve



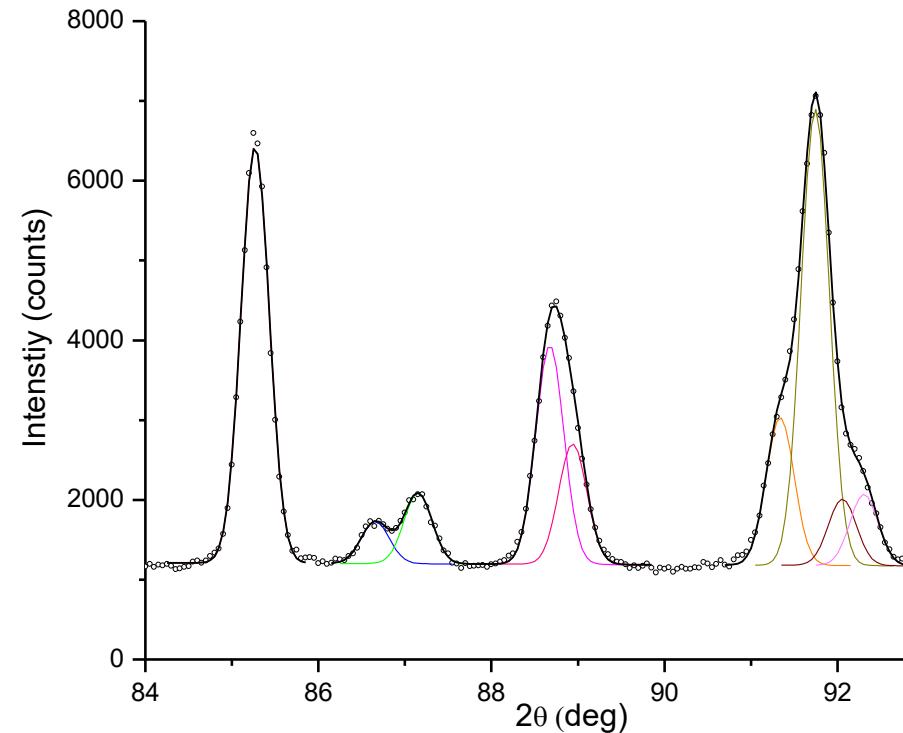
# The Rietveld method

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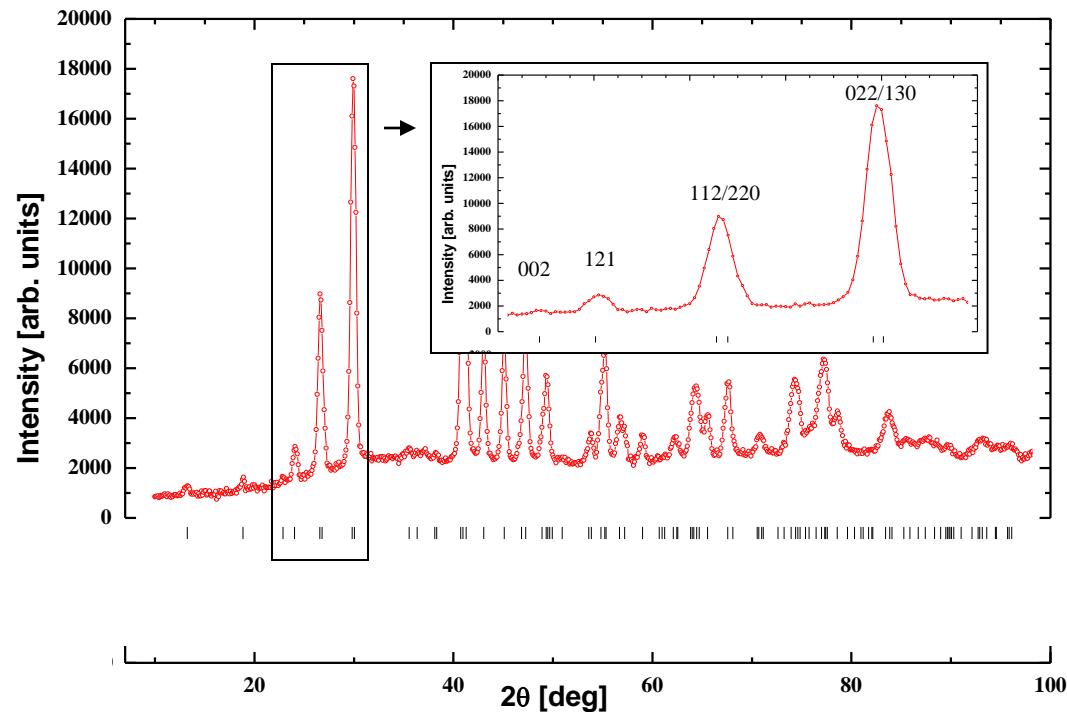


The Gaussian curve



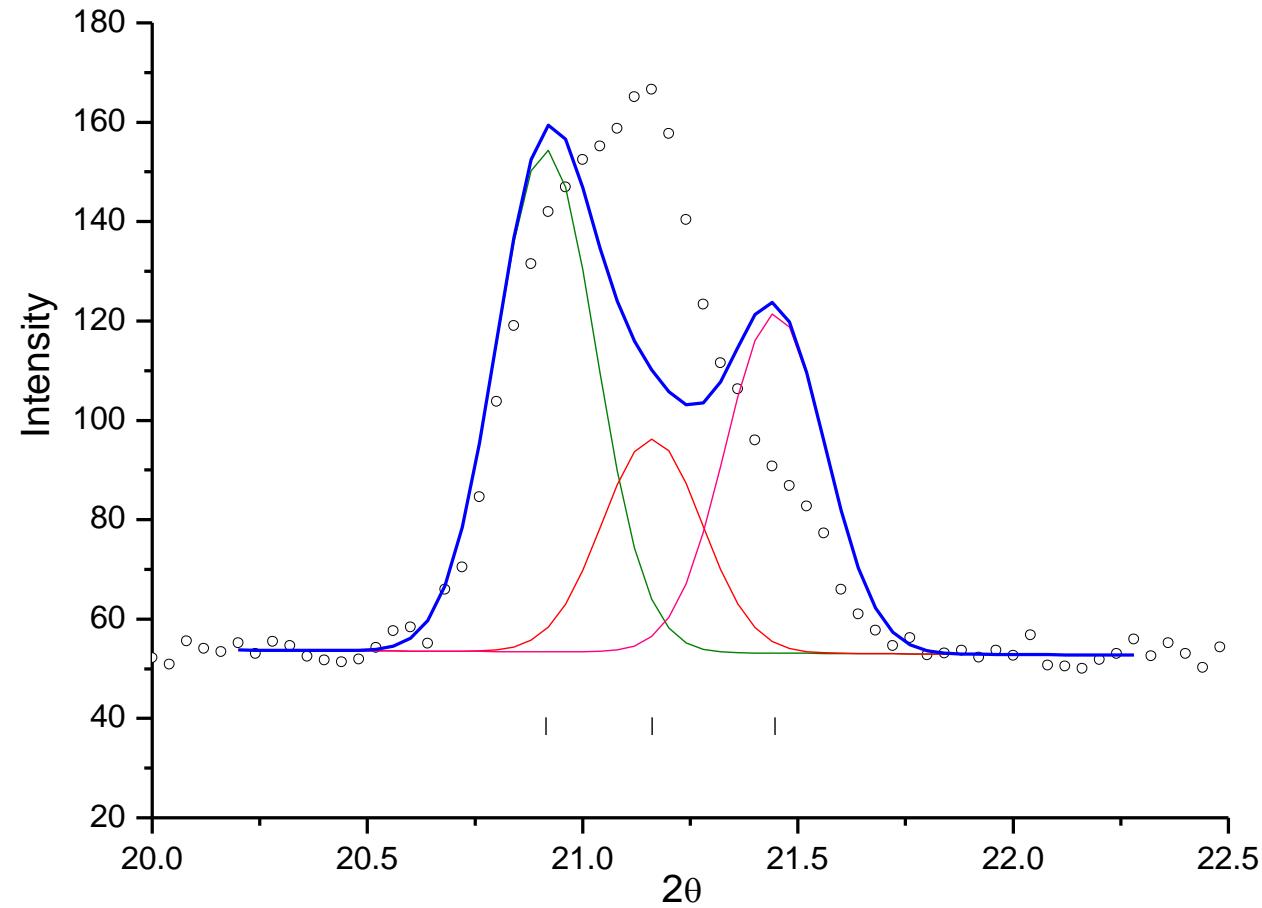
# The Rietveld method

- Developed as a technique for *structure refinement*.

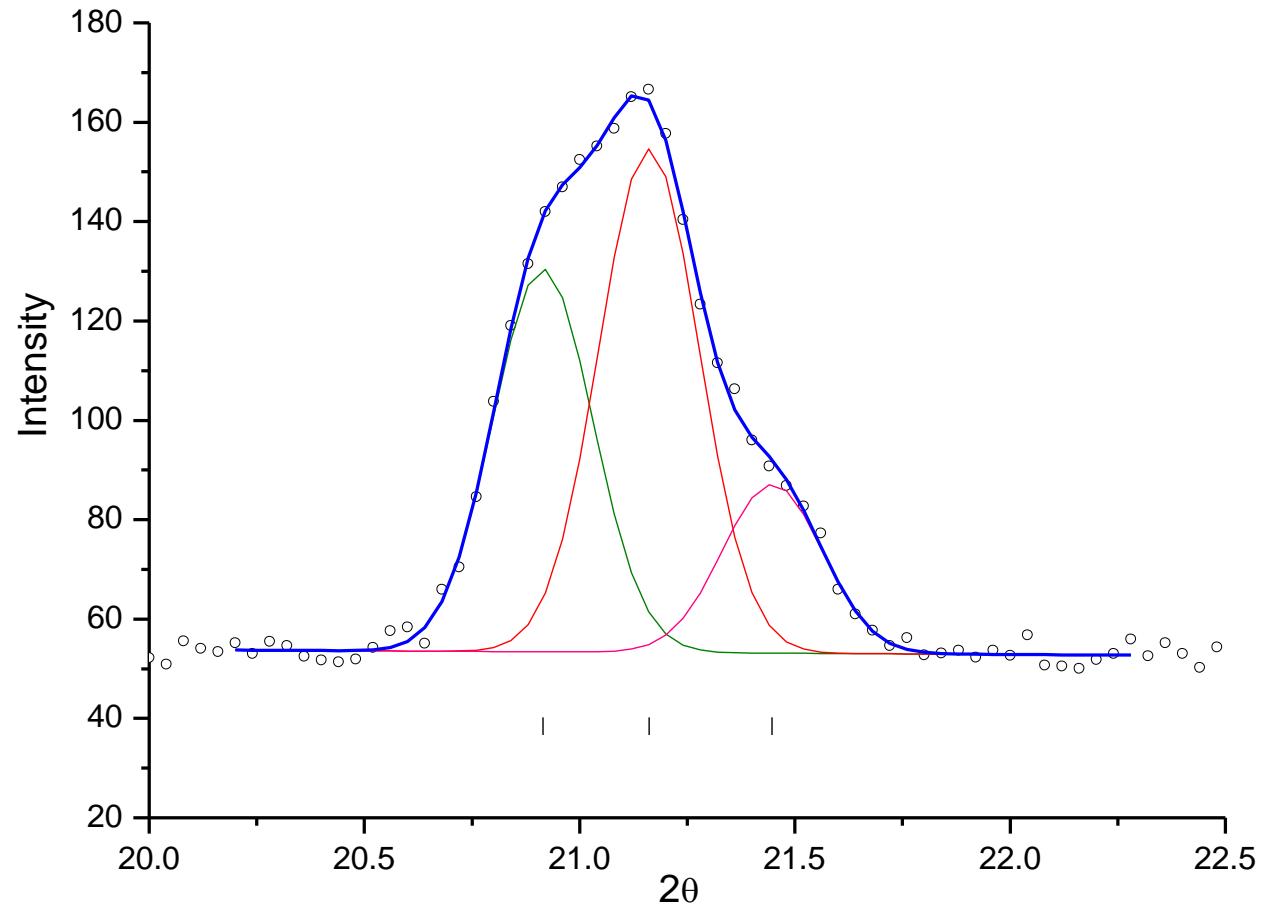


Rietveld's idea:  
Why not fit the entire calculated profile from the model to the data, instead of just the integrated intensities?

# The Rietveld method

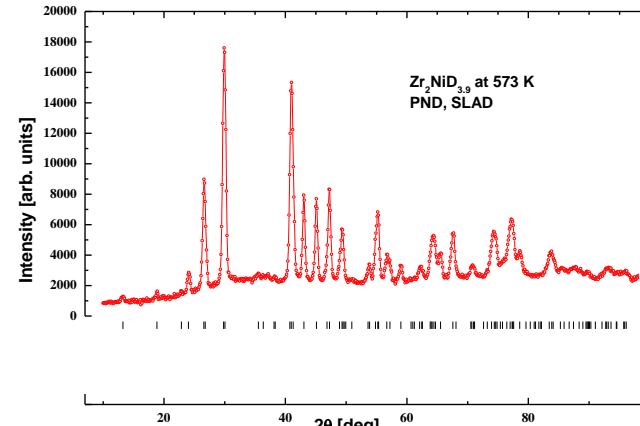


# The Rietveld method



# The Rietveld method

## The calculated profile



$$y_i^{calc} = s \sum_K L_K |F_K|^2 \phi(2\theta_i - 2\theta_K) P_K A + y_i^{background}$$

calculated  
intensity in  
point *i*

# The Rietveld method

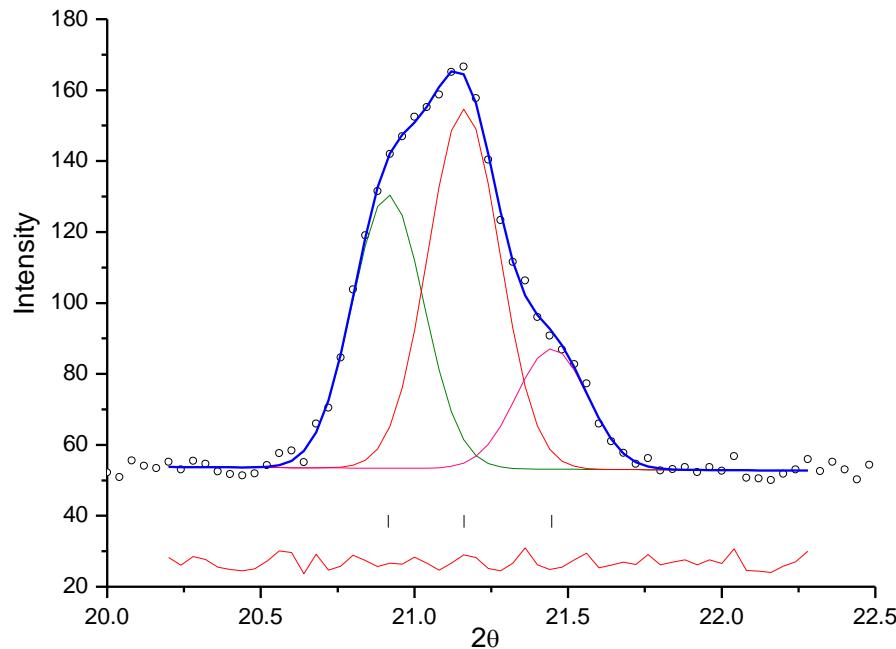
## The calculated profile

$$y_i^{calc} = s \sum_K L_K |F_K|^2 \phi(2\pi \sin(\theta)/\lambda)$$

scale factor

calculated intensity in point  $i$

Sum over all Bragg peaks,  $K$ , that contribute with intensity to point  $i$



# The Rietveld method

## The calculated profile

$$y_i^{calc} = s \sum_K L_K |F_K|^2 \phi(2\theta_i - 2\theta_K) P_K A + y_i^{background}$$

calculated intensity in point  $i$

scale factor

Lorentz factor and multiplicity

Sum over all Bragg peaks,  $K$ , that contribute with intensity to point  $i$

The profile function

preferred orientation

absorption

background

The square modulus of the structure factor for Bragg peak  $K$

The diagram illustrates the components of the Rietveld calculated profile equation. The equation is:

$$y_i^{calc} = s \sum_K L_K |F_K|^2 \phi(2\theta_i - 2\theta_K) P_K A + y_i^{background}$$

The components are labeled as follows:

- $y_i^{calc}$ : calculated intensity in point  $i$
- $s$ : scale factor
- $L_K$ : Lorentz factor and multiplicity
- $|F_K|^2$ : The square modulus of the structure factor for Bragg peak  $K$
- $\phi(2\theta_i - 2\theta_K)$ : The profile function
- $P_K$ : preferred orientation
- $A$ : absorption
- $y_i^{background}$ : background

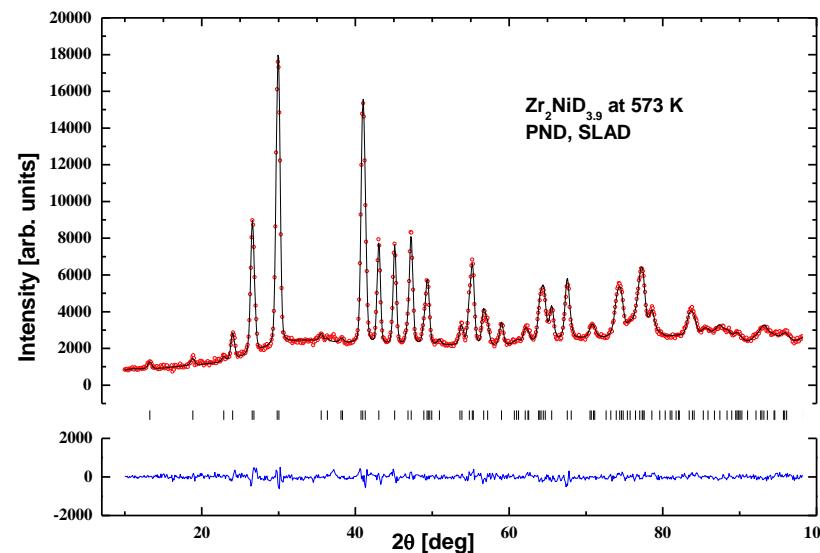
# The Rietveld method

## Fitting the profile

$$y_i^{calc} = s \sum_K L_K |F_K|^2 \phi(2\theta_i - 2\theta_K) P_K A + y_i^{background}$$

The parameters in  $y_i^{calc}$  undergo a *least-square refinement* to minimize  $R_{wp}$

$$R_{wp} = \sqrt{\frac{\sum_i w_i (y_i^{obs} - y_i^{calc})^2}{\sum_i w_i (y_i^{obs})^2}}$$



# The Rietveld method

## The structure factor

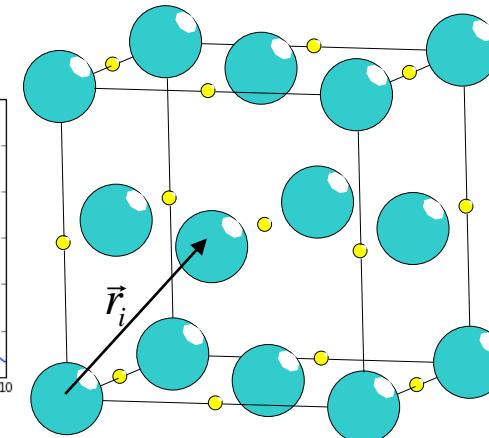
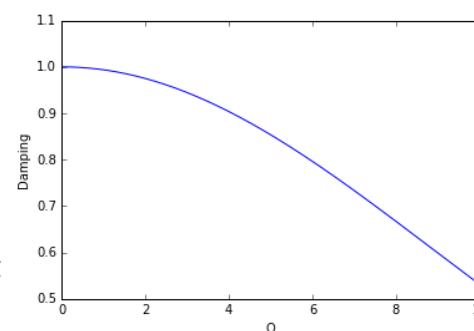
$$y_i^{calc} = s \sum_K L_K |F_K|^2 \phi(2\theta_i - 2\theta_K) P_K A + y_i^{background}$$

$$|F_K|^2 = \left| \sum_i b_i \cdot e^{2\pi i (\vec{r}_i \cdot \vec{K})} \right|^2 = \left| \sum_i b_i \cdot e^{2\pi i (hx_i + ky_i + lz_i)} \right|^2$$

$$b(\theta) = b \cdot e^{-B \left( \frac{\sin \theta}{\lambda} \right)^2}$$

The displacement factor

$B = 8\pi^2 U$  The mean square shift  
of the atom from its equilibrium position.



# The Rietveld method

## The profile function

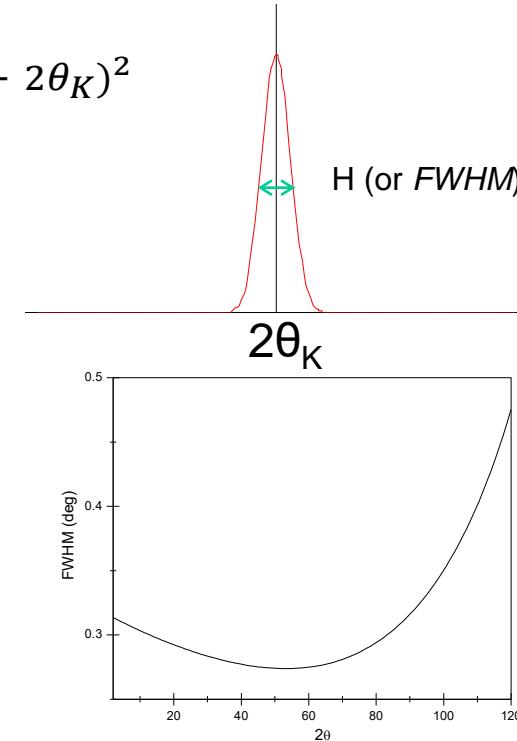
$$y_i^{calc} = s \sum_K L_K |F_K|^2 \phi(2\theta_i - 2\theta_K) P_K A + y_i^{background}$$

Gaussian:  $\phi(2\theta_i - 2\theta_K)_{gauss} = \frac{2\sqrt{\ln 2}}{H\sqrt{\pi}} e^{\frac{-4\ln 2}{H^2}(2\theta_i - 2\theta_K)^2}$

H varies with  $2\theta$ !

Caglioti equation:  $H = \sqrt{(U \tan^2 \theta + V \tan \theta + W)}$

Refineable parameters

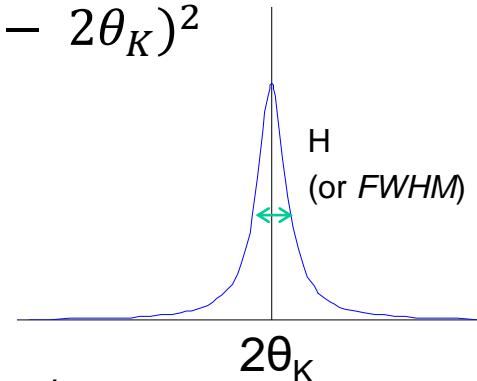


# The Rietveld method

## The profile function

$$y_i^{calc} = s \sum_K L_K |F_K|^2 \phi(2\theta_i - 2\theta_K) P_K A + y_i^{background}$$

Lorentzian:  $\phi(2\theta_i - 2\theta_K)_{Lorentz} = \frac{2\sqrt{\ln 2}}{H\pi} \frac{1}{1 + \frac{4}{H^2} (2\theta_i - 2\theta_K)^2}$



pseudo-Voigt:  $\phi(2\theta_i - 2\theta_K)_{pseudo-Voigt} = \eta \cdot \phi_{Lorentz} + (1-\eta) \cdot \phi_{Gauss}$

$$H = \sqrt{(U \tan^2 \theta + V \tan \theta + W)}$$

Refineable parameter

Fullprof: Npr = 5  
GSAS: N.A.

# The Rietveld method

## Sample contributions to the profile function

Broadening due to particle size:  $\beta_{size} = \frac{\lambda K}{D \cos \theta} \propto \frac{1}{\cos \theta}$  Scherrer equation

«Particle size» (volume-weighted average size of coherent domains)

Mostly lorentzian

Broadening due to strain:  $\beta_{strain} = B\varepsilon \tan \theta \propto \tan \theta$

strain

Mostly gaussian

$$H = \sqrt{(U \tan^2 \theta + V \tan \theta + W)}$$

$$\phi(2\theta_i - 2\theta_K)_{pseudo-Voigt} = \eta \cdot \phi_{lorentz} + (1-\eta) \cdot \phi_{gauss}$$

# The Rietveld method

## The Thompson-Cox-Hastings pseudo-Voigt

$$H_{gauss} = \sqrt{(U \tan^2 \theta + V \tan \theta + W + \frac{Z}{\cos^2 \theta})}$$
$$H_{lorentz} = X \tan \theta + \frac{Y}{\cos \theta}$$

Strain-dependent      Sample independent!

Size-dependent

$$\beta_{size} \propto \frac{1}{\cos \theta}$$

Mostly lorentzian

$$\beta_{strain} \propto \tan \theta$$

Mostly gaussian

Fullprof: Npr = 7

GSAS: type 2

# The (Thompson-Cox-Hastings) pseudo-Voigt

Fullprof

```
!-----> Profile Parameters for Pattern # 1
! Scale      Shape1     Bov      Str1      Str2      Str3      Strain-Model
0.38120    0.00000    0.00000    0.00000    0.00000    0.00000    0
11.00000    0.00000    0.00000    0.00000    0.00000    0.00000    0
! U          V          W          X          Y          GauSiz    LorSiz Size-Model
0.361019   -0.551548   0.335122   0.000000   0.000000   0.000000   0.000000   0
0.00000    0.00000    0.00000    0.00000    0.00000    0.00000    0.00000    0
! a          b          c          alpha     beta      gamma    #Cell Info
7.633083   7.633083   6.520463   90.000000  90.000000  90.000000  0.000000
81.00000   81.00000  101.00000  0.000000   0.000000   0.000000   0.000000
```

\*10000/(2.35<sup>2</sup>)

Z

GSAS

Hist 1 -- Phase 1 (type 2)				
		Damping	Peak cutoff	Change Type
GU	<input checked="" type="checkbox"/>	0.691440E+03	GV	-0.845000E+03
LX	<input checked="" type="checkbox"/>	0.258394E+02	LY	0.000000E+00
as	<input checked="" type="checkbox"/>	0.150000E+02	GW	0.451000E+03
stec	<input type="checkbox"/>	0.000000E+00	LY	0.000000E+00
L11	<input type="checkbox"/>	0.000000E+00	trns	0.000000E+00
L12	<input type="checkbox"/>	0.000000E+00	GP	0.000000E+00
			sfec	0.000000E+00
			L33	0.000000E+00
			L22	0.000000E+00
			L13	0.000000E+00
			L23	0.000000E+00

$$H_{gauss} = \sqrt{(U \tan^2 \theta + V \tan \theta + W + \frac{Z}{\cos^2 \theta})}$$

$$H_{lorentz} = X \tan \theta + \frac{Y}{\cos \theta}$$

Sample independent!

Strain-dependent

Size-dependent

# Evaluating the fit

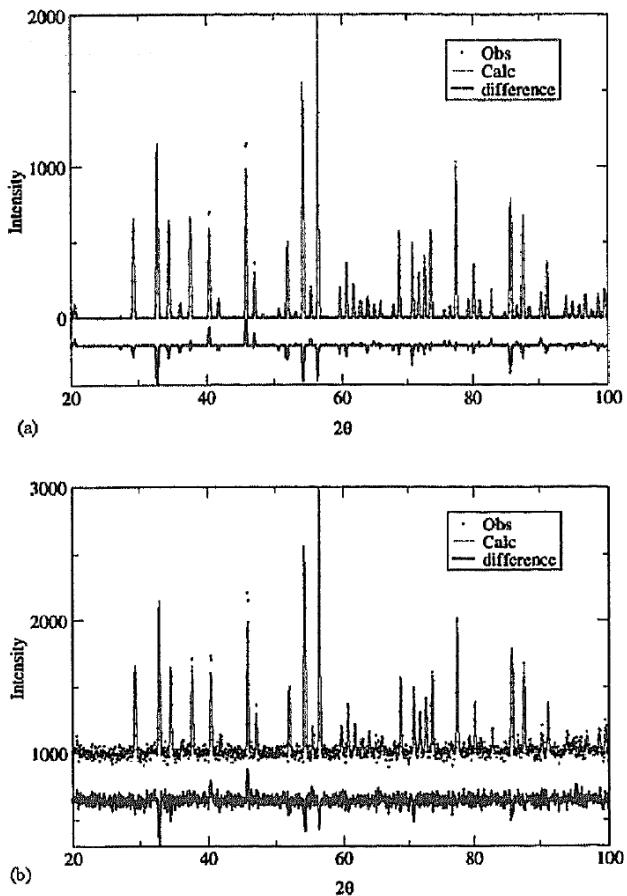


Figure 1. A demonstration of the effect of background on a Rietveld fit. Two simulated fits are shown, where the models have the same discrepancies from the simulated data and where the Bragg intensities and counting times are equivalent. However, in case (a) no background is present,  $R_{wp}=23\%$  and  $\chi^2=2.54$ , while in case (b), significant background is present,  $R_{wp}=3.5\%$  and  $\chi^2=1.31$ .

$$R_{wp} = \sqrt{\frac{\sum_i w_i (y_i^{obs} - y_i^{calc})^2}{\sum_i w_i (y_i^{obs})^2}}$$

Most often used. But can be highly influenced by factors that do not imply a poor structure model.

$$\chi^2 = \frac{R_{wp}}{R_{exp}} \quad R_{exp} = \sqrt{\frac{N}{\sum_i w_i (y_i^{obs})}}$$

Should be close to 1 when there are no systematic errors in the model, but in many cases that's not possible.

# Evaluating the fit

## **R factors in Rietveld analysis: How good is good enough?**

Brian H. Toby

*BESSRC/XOR, Advanced Photon Source, Argonne National Laboratory, Argonne, Illinois*

Powder Diffraction **21** (1), March 2006

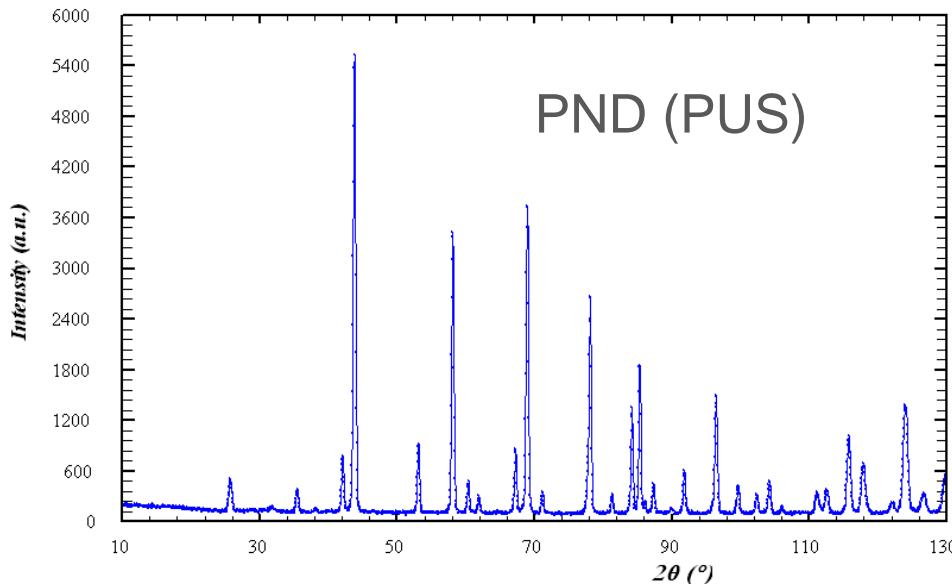
In my experience, the most important way to determine the quality of a Rietveld fit is by viewing the observed and calculated patterns graphically and to ensure that the model is chemically plausible.

# The Rietveld method

## Joint exercise

Approximate model of  $\text{Al}_2\text{O}_3$ :

- Trigonal, space group R –3 c
- $a \sim 4.75 \text{ \AA}$ ,  $c \sim 12.99 \text{ \AA}$
- Al in  $0\ 0\sim0.35$   
O in  $\sim0.29\ 0\ \frac{1}{4}$



We want a more accurate structure model!

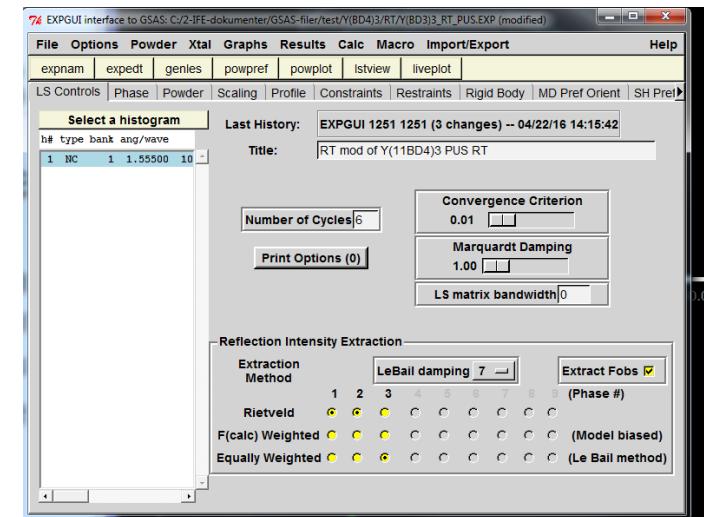
# Le Bail refinements

## «structureless Rietveld»

- Bragg peak positions are calculated from unit cell and space group, but all intensities can vary freely.
- Good for checking the unit cell
- ... or to refine the profile parameter if the structure model is bad.

```
!-----  
! Data for PHASE number: 1 ==> Current R_Bragg for Pattern# 1: 10.63  
!-----  
Th2AlD4  
!  
!Nat Dis Ang Pr1 Pr2 Pr3 Jbt Irf Isy Str Furth      ATZ      Nvk Npr More  
 3   0   0 1.0 0.0 5.0  2   0   0   0   0   1996.359  0   7   1  
!
```

Jbt = 0 : Rietveld  
Jbt = 2 : Le Bail («profile matching）



# Conclusion

- Rietveld refinement is an effective technique to refine crystal structure models against powder diffraction data.
- It can also be used for quantitative phase analysis and to extract microstructural information.
- It requires active participation from the user. It's not a black-box technique!